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# On the Dynamics of Continuous Distributions of Dislocations

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## Abstract

For materials with a continuous distribution of dislocations, equations of motion are derived from a symplectic structure on an appropriate configuration space. The proposed dynamics generalizes from elasticity.

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## 1 Introduction

A mathematical framework for the dynamics of an elastic material is given by the space of all embeddings  $E(M; \mathbb{R}^3)$  of a reference body  $M$  into the physical space  $\mathbb{R}^3$ . The constitutive law determining the equations of evolution can be given in terms of a virtual work functional on this phase space, cf. [8]. The invariance of the system under rigid global translations implies that the differential  $dj$  of the embedding  $j \in E(M; \mathbb{R}^3)$  is the essential quantity for the constitutive behaviour of the material, cf. [3]. In classical terms this differential is precisely the deformation gradient of the actual configuration of the system. Mathematically the deformation gradient  $dj$  may be considered as an exact ( $\mathbb{R}^3$ -valued) differential one-form in  $\Omega^1(M; \mathbb{R}^3)$ .

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In the continuum theory of defects one describes dislocations by a torsion density on the reference body, cf. [9, 15, 19]. This torsion density may be identified with an exact ( $\mathbb{R}^3$ -valued) differential two-form  $d\gamma \in \Omega^2(M; \mathbb{R}^3)$ . The corresponding Burgers vector computes as the integral of  $d\gamma$  over a bounded surface  $S \subset M$ , cf. [20].

To incorporate this description of dislocations into the framework of elasticity, the Helmholtz decomposition theorem is utilized which claims that any differential form may be uniquely decomposed into a gradient and a divergence-free part. A generalised configuration space for a material with dislocations  $\mathcal{V}(M; \mathbb{R}^3)$  is defined as a submanifold of  $\Omega^1(M; \mathbb{R}^3)$ . Each generalised configuration  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$  splits into an elastic or gradient part  $dj$ , where  $j \in E(M; \mathbb{R}^3)$  is an embedding, and into a so-called plastic part  $\beta$  describing the dislocation density, cf. [20].

The main objective of this paper is to derive a dynamics for a material with a continuous distribution of dislocations. This is done by introducing a symplectic structure  $\Omega$  and a kinetic energy functional  $\mathcal{E}$  on the tangent space  $T\mathcal{V}(M; \mathbb{R}^3)$  of the configuration space  $\mathcal{V}(M; \mathbb{R}^3)$ . The constitutive behaviour of such a system is described by a virtual work functional  $F$  on  $\mathcal{V}(M; \mathbb{R}^3)$ . The resulting principle of virtual work determines weak equations of motion for the generalised configurations  $\gamma$ .

Using the Helmholtz decomposition theorem, these equations split into a part which determines the evolution of the elastic parts  $dj$  of a generalised configuration  $\gamma$  and into a part which determines the evolution of the plastic parts  $\beta$ . The equations for the elastic parts are just the well-known equations in classical elasticity. Thus, for purely elastic materials, this approach covers the classical theory.

## 2 Differential Forms

Since in this approach towards a dynamics of dislocations, differential forms provide a convenient framework, a brief introduction is given. Let  $M$  be the *body manifold* in the sense of elasticity. Assume that  $M$  is a smooth connected 3-dimensional compact oriented Riemannian manifold with boundary which is embedable into the physical space  $\mathbb{R}^3$ . A  $\mathbb{R}^3$ -valued differential form  $\omega \in \Omega^k(M; \mathbb{R}^3)$  of degree  $k$  is a smooth assignment of a skew-symmetric  $k$ -linear map  $\omega_p$  on  $T_p M$  to each point  $p \in M$ , where

$$\omega_p : \underbrace{T_p M \times \cdots \times T_p M}_{k\text{-times}} \longrightarrow \mathbb{R}^3 \quad \forall p \in M.$$

In classical terms, differential forms may be considered as skew-symmetric two-point tensors of type  $(1, k)$  on the body manifold  $M$  which are well-known objects in continuum mechanics, cf. [12]. Of particular interest in our approach are the cases  $k = 0, 1, 2$ . For example, the deformation gradient and the first Piola-Kirchhoff stress tensor are

considered here as  $\mathbb{R}^3$ -valued one-forms on the body manifold  $M$ , i.e. as some  $\omega \in \Omega^1(M; \mathbb{R}^3)$ . Analogously, placements of  $M$  and force fields are elements in  $\Omega^0(M; \mathbb{R}^3)$  which, by definition, is equal to  $C^\infty(M; \mathbb{R}^3)$ .

Each  $\Omega^k(M; \mathbb{R}^3)$  may be equipped with a fibre metric by using the Riemannian metric  $g$  on  $M$  and the standard scalar product  $\langle \cdot, \cdot \rangle_{\mathbb{R}^3}$  on  $\mathbb{R}^3$ . For our purposes, it suffices to consider the cases  $k = 0, 1$ . Let  $E_1, E_2, E_3 \in \Gamma(TM)$  be a triple of vector fields orthonormal with respect to the metric  $g$ . A fibre metric on  $\Omega^1(M; \mathbb{R}^3)$  is then defined by

$$\langle \omega, \eta \rangle := \sum_i \langle \omega(E_i), \eta(E_i) \rangle_{\mathbb{R}^3}, \quad \omega, \eta \in \Omega^1(M; \mathbb{R}^3). \quad (1)$$

The product (1) does only depend on the metric  $g$  but not on the chosen frame on  $M$ , cf. [13]. Notice that (1) corresponds to the contraction of skew symmetric two-point tensors. If  $e_1, e_2, e_3 \in \mathbb{R}^3$  denotes the standard basis in  $\mathbb{R}^3$  and  $\theta^1, \theta^2, \theta^3 \in \Omega^1(M)$  the dual frame corresponding to  $E_1, E_2, E_3$ , then, in coordinates, any one-forms  $\omega$  and  $\eta$  may be written as  $\omega = \sum_{L,l} \omega_l^L \theta^l e_L$  and  $\eta = \sum_{L,l} \eta_l^L \theta^l e_L$ . Thus (1) reads

$$\langle \omega, \eta \rangle = \sum_{L,l=1}^3 \omega_l^L \eta_l^L.$$

With the help of the Riemannian volume element  $\mu$  induced by  $g$ , the space  $\Omega^1(M; \mathbb{R}^3)$  is now endowed with an  $L^2$ -product  $\mathcal{G}$ , given by

$$\mathcal{G}(\omega, \eta) := \int_M \langle \omega, \eta \rangle \mu, \quad \omega, \eta \in \Omega^1(M; \mathbb{R}^3). \quad (2)$$

For  $k = 0$  the corresponding  $L^2$ -product  $\mathcal{G}$  is just the usual one. Let  $\nabla$  denote the Levi-Civita connection on  $M$  associated to  $g$ . Then  $\nabla$  induces a *covariant derivative* on  $\Omega^1(M; \mathbb{R}^3)$ , given by

$$(\nabla_Y \omega)(X) = D[\omega(X)](Y) - \omega(\nabla_Y X), \quad X, Y \in \Gamma(TM).$$

Here, the first term of the right hand side means the directional derivative of the  $\mathbb{R}^3$ -valued function  $\omega(X)$  in direction of the vector field  $Y$ . For  $k = 0$  the second term of the right hand side of the above expression vanishes. The covariant derivative allows to write the *exterior derivative*  $d : \Omega^1(M; \mathbb{R}^3) \rightarrow \Omega^2(M; \mathbb{R}^3)$  as

$$d\omega(X, Y) = (\nabla_X \omega)(Y) - (\nabla_Y \omega)(X), \quad X, Y \in \Gamma(TM).$$

For  $k = 0$  the exterior derivative corresponds to the gradient. The *co-differential*  $\delta : \Omega^1(M; \mathbb{R}^3) \rightarrow \Omega^0(M; \mathbb{R}^3)$  may be defined by

$$\delta\omega := - \sum_{i=1}^3 (\nabla_{E_i} \omega)(E_i).$$

Notice that the co-differential  $\delta$ , unlike the exterior derivative, depends on the chosen Riemannian metric  $g$ . In classical tensor notation,  $\delta$  corresponds to the divergence of a tensor field.

Let  $\mathcal{N}$  denote the outward pointing unit normal field on the boundary  $\partial M$  of  $M$ . A differential one-form  $\omega$  is called *parallel* to  $\partial M$  iff its normal component vanishes, that is  $\omega(\mathcal{N}) = 0$ . Define the space of all divergence-free and parallel one-forms by

$$\mathcal{D}(M; \mathbb{R}^3) := \{ \omega \in \Omega^1(M; \mathbb{R}^3) \mid \delta\omega = 0 \text{ and } \omega(\mathcal{N}) = 0 \}.$$

We are now able to state the *Helmholtz decomposition* for the special case of  $\mathbb{R}^3$ -valued one-forms. For a general proof see [17].

**Theorem 2.1 HELMHOLTZ DECOMPOSITION**

Let  $M$  be a compact, oriented Riemannian manifold with boundary. Then for any  $\omega \in \Omega^1(M; \mathbb{R}^3)$  there exist  $\theta \in \Omega^0(M; \mathbb{R}^3)$  and  $\beta \in \mathcal{D}(M; \mathbb{R}^3)$  such that  $\omega = d\theta + \beta$ . Moreover,  $d\theta$  and  $\beta$  are mutually  $L^2$ -orthogonal with respect to the inner product (2), that is the decomposition

$$\Omega^1(M; \mathbb{R}^3) = d\Omega^0(M; \mathbb{R}^3) \oplus \mathcal{D}(M; \mathbb{R}^3)$$

is direct and  $L^2$ -orthogonal.

### 3 The Kinematics of Dislocations

Let  $j : M \rightarrow \mathbb{R}^3$  be a smooth embedding of the body manifold  $M$  into the Euclidean space  $\mathbb{R}^3$ , and  $E(M; \mathbb{R}^3)$  denote the space of all such embeddings<sup>1</sup>. In pure elasticity  $E(M; \mathbb{R}^3)$  constitutes the configuration space of the system; in classical terms its elements  $j$  are called placement (or transplacement) fields. The displacement fields  $u \in C^\infty(M; \mathbb{R}^3)$  compute as  $u = (j - j_0)$ , where  $j_0$  is a reference configuration.

This section is aimed at generalising the classical configuration space  $E(M; \mathbb{R}^3)$  in such a way that the description of the kinematics of dislocations is included. We introduce a configuration space for an elastic solid whose internal structure is characterised by a frame, i.e. a triple of linear independent vector fields on  $M$

$$Y_1, Y_2, Y_3 \in \Gamma(TM). \tag{3}$$

Physically, these vector fields describe lattice vectors of a continued crystal as worked out in [9]. We denote the standard basis of  $\mathbb{R}^3$  by  $e_1, e_2, e_3$ . Since  $M$  is embedable

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<sup>1</sup> $E(M; \mathbb{R}^3)$  is an open subset in the Fréchet space  $C^\infty(M; \mathbb{R}^3)$ , see [2] for details.

into  $\mathbb{R}^3$ , for any arbitrary frame (3), there exists a unique fibrewise one-to-one map  $\gamma : TM \rightarrow \mathbb{R}^3$  such that

$$\gamma_p(Y_i(p)) = e_i, \quad i = 1, 2, 3 \quad \forall p \in M. \quad (4)$$

Mathematically,  $\gamma$  is a  $\mathbb{R}^3$ -valued one-form  $\gamma \in \Omega^1(M; \mathbb{R}^3)$  on  $M$  which is fibrewise one-to-one. The set of all these one-forms is defined by

$$\mathcal{I}(M; \mathbb{R}^3) := \left\{ \gamma \in \Omega^1(M; \mathbb{R}^3) \mid \gamma_p : T_p M \rightarrow \mathbb{R}^3 \text{ is one-to-one, } p \in M \right\}.$$

Consider a fixed  $\gamma \in \mathcal{I}(M; \mathbb{R}^3)$ . Then  $\gamma(X) \in C^\infty(M; \mathbb{R}^3)$  is a smooth function for each  $X \in \Gamma(TM)$ . Let  $D(\gamma(X))(Y)$  denote the directional derivative of  $\gamma(X)$  into the direction of some  $Y \in \Gamma(TM)$ . A connection  $\nabla[\gamma]$  on  $TM$  associated with  $\gamma \in \mathcal{I}(M; \mathbb{R}^3)$  is then defined by

$$\nabla[\gamma]_Y X = \gamma^{-1} D(\gamma(X))(Y), \quad X, Y \in \Gamma(TM). \quad (5)$$

In a coordinate system on  $M$ , the Christoffel symbols of (5) read

$$\Gamma_{lm}^k = \sum_{L=1}^3 (\gamma^{-1})_L^k \partial_l \gamma_m^L.$$

It is easy to verify that the curvature of this connection vanishes, i.e. the connection (5) is flat. Conversely, it is shown in [20] that for any flat connection  $\widetilde{\nabla}$  on  $TM$ , there is some  $\gamma \in \mathcal{I}(M; \mathbb{R}^3)$  with  $\widetilde{\nabla} = \nabla[\gamma]$ . The torsion  $T^\nabla$  of an arbitrary connection  $\nabla$  is defined by

$$T^\nabla(X, Y) = \nabla_Y X - \nabla_X Y - [X, Y] \quad \forall X, Y \in \Gamma(TM).$$

In particular, if  $T[\gamma]$  denotes the torsion of  $\nabla[\gamma]$ , it follows from (5) and the definition of the exterior derivative  $d$  that

$$d\gamma(X, Y) = \gamma(T[\gamma](X, Y)), \quad X, Y \in \Gamma(TM).$$

In classical terms, the torsion of a connection describes the *dislocation density* or the *material inhomogeneity* of a material. Since  $\gamma$  is fibrewise one-to-one, the discussion shows that  $T[\gamma] = \gamma^{-1} d\gamma$ . Therefore, the dislocation density  $T[\gamma]$  might as well be measured by the exterior derivative of the one-form  $\gamma \in \mathcal{I}(M; \mathbb{R}^3)$ . Hence, the two-form  $d\gamma$  will be referred to as a dislocation density of the material. In particular,

$$d\gamma = 0 \quad \iff \quad T[\gamma] = 0,$$

implying that the material is defect-free if and only if  $\gamma$  is closed, i.e.  $d\gamma = 0$ . The Burgers vector  $b$  of an arbitrary surface  $S \subset M$  associated with the dislocation density  $d\gamma$  computes as the integral

$$b = \int_S d\gamma.$$

The crucial observation is that according to the *Helmholtz decomposition*, Theorem 2.1, each  $\gamma \in \mathcal{I}(M; \mathbb{R}^3)$  uniquely splits into

$$\gamma = dv + \beta, \quad \text{where} \quad dv \in d\Omega^0(M; \mathbb{R}^3), \quad \beta \in \mathcal{D}(M; \mathbb{R}^3). \quad (6)$$

Since  $d^2 = 0$ , only the divergence-free part  $\beta \in \mathcal{D}(M; \mathbb{R}^3)$  of  $\gamma$  contributes to the dislocation density. In particular  $d\gamma = d\beta$ , i.e. the dislocation density is uniquely determined by the so-called non-exact component  $\beta$ .

As far as classical elasticity is concerned, the essential quantity for the constitutive behaviour of a material is the deformation gradient  $dj \in \Omega^1(M; \mathbb{R}^3)$  of an actual embedding  $j \in E(M; \mathbb{R}^3)$ . It is shown in [3] that the set of all such gradients

$$dE(M; \mathbb{R}^3) = \{dj \mid j \in E(M; \mathbb{R}^3)\}$$

is an open subset of the Fréchet space of all one-forms  $\Omega^1(M; \mathbb{R}^3)$ . Since differentials of embeddings are fibrewise one-to-one, we have  $dE(M; \mathbb{R}^3) \subset \mathcal{I}(M; \mathbb{R}^3)$ . Each deformation gradient  $dj \in dE(M; \mathbb{R}^3)$  defines a frame  $X_1, X_2, X_3 \in \Gamma(TM)$  by solving

$$dj(X_l) = e_l, \quad l = 1, 2, 3. \quad (7)$$

Since  $d^2 = 0$ , it follows from (4) that this triple of vector fields characterises a defect-free material. Therefore, a placement  $j \in E(M; \mathbb{R}^3)$  will be called *integrable configuration* of the body manifold  $M$ ; an arbitrary  $\gamma \in \mathcal{I}(M; \mathbb{R}^3)$  will be referred to as a *generalised configuration* of  $M$ .

According to [18] the evolution of defects is held responsible for the discrepancy between the macroscopic deformation and the behaviour of the lattice. Therefore, we think of the component  $\beta \in \mathcal{D}(M; \mathbb{R}^3)$  as a quantity by which the frame  $X_1, X_2, X_3$  is *incompatibly* deformed. The vector fields

$$(dj + \beta)(X_1), (dj + \beta)(X_2), (dj + \beta)(X_3)$$

constitute a frame on  $j(M) \subset \mathbb{R}^3$  if and only if  $dj + \beta$  is injective. For  $\beta \neq 0$ , this frame represents a dislocated lattice on the embedded body.

The general idea is that only the integrable part, i.e. the gradient part of a generalised configuration  $\gamma \in \mathcal{I}(M; \mathbb{R}^3)$  becomes visible as a placement of the body manifold in Euclidean space. Thus, we consider generalised configurations  $\gamma = dj + \beta \in \mathcal{I}(M; \mathbb{R}^3)$  whose integrable part  $dj$  stems from a placement  $j \in E(M; \mathbb{R}^3)$  and whose non-integrable part  $\beta$  lies in  $\mathcal{D}(M; \mathbb{R}^3)$ . The set of all such configurations is denoted by

$$\mathcal{V}(M; \mathbb{R}^3) = \{dj + \beta \in \mathcal{I}(M; \mathbb{R}^3) \mid j \in E(M; \mathbb{R}^3), \beta \in \mathcal{D}(M; \mathbb{R}^3)\}.$$

Observe that by construction  $\mathcal{V}(M; \mathbb{R}^3) \subset \mathcal{I}(M; \mathbb{R}^3)$ , where the exact parts of generalised configurations  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$  are restricted to embeddings  $j \in E(M; \mathbb{R}^3)$ . Since  $\mathcal{V}(M; \mathbb{R}^3)$  is an open Fréchet submanifold of  $\Omega^1(M; \mathbb{R}^3)$ , we take  $\mathcal{V}(M; \mathbb{R}^3)$  as a configuration space for an elastic material which possibly may be dislocated, cf. [20].

## 4 The Geometry of $\mathcal{V}(M; \mathbb{R}^3)$

For a mathematical formulation of a dynamic theory of dislocated materials, a metric on the configuration space  $\mathcal{V}(M; \mathbb{R}^3)$  is needed. Following [6], we first introduce an appropriate metric on  $dE(M; \mathbb{R}^3)$ . Let  $\rho : M \rightarrow \mathbb{R}$  be a strictly positive real-valued function which physically may be thought of as the mass distribution of the material. Since  $E(M; \mathbb{R}^3)$  is open in  $C^\infty(M; \mathbb{R}^3)$ , the tangent manifold of  $E(M; \mathbb{R}^3)$  is trivial

$$TE(M; \mathbb{R}^3) = E(M; \mathbb{R}^3) \times C^\infty(M; \mathbb{R}^3).$$

Identifying each tangent vector with its principal part, a metric on  $E(M; \mathbb{R}^3)$  is defined by setting

$$\mathcal{G}_\rho(u_1, u_2) := \int_M \rho \langle u_1, u_2 \rangle_{\mathbb{R}^3} \mu, \quad u_1, u_2 \in C^\infty(M; \mathbb{R}^3). \quad (8)$$

Using (8), each  $j \in E(M; \mathbb{R}^3)$  and each  $u \in C^\infty(M; \mathbb{R}^3)$  may be decomposed into

$$j = j^0 + C_j, \quad \text{where } C_j \in \mathbb{R}^3, \quad \mathcal{G}_\rho(j^0, c) = 0 \quad \forall c \in \mathbb{R}^3$$

and

$$u = u^0 + C_u, \quad \text{where } C_u \in \mathbb{R}^3, \quad \mathcal{G}_\rho(u^0, c) = 0 \quad \forall c \in \mathbb{R}^3$$

respectively. The sets

$$E_0(M; \mathbb{R}^3) := \left\{ j \in E(M; \mathbb{R}^3) \mid \int_M \rho j \mu = 0 \right\}$$

and

$$C_0^\infty(M; \mathbb{R}^3) := \left\{ u \in C^\infty(M; \mathbb{R}^3) \mid \int_M \rho u \mu = 0 \right\}$$

are Fréchet manifolds which are naturally isomorphic to  $dE(M; \mathbb{R}^3)$  and  $d\Omega^0(M; \mathbb{R}^3)$  respectively, cf. [3, 4]. Since  $dE(M; \mathbb{R}^3) \subset d\Omega^0(M; \mathbb{R}^3)$  is open,

$$T(dE(M; \mathbb{R}^3)) = dE(M; \mathbb{R}^3) \times d\Omega^0(M; \mathbb{R}^3).$$

Configurations in  $j \in E_0(M; \mathbb{R}^3)$  are such that the center of mass is kept fixed,  $C_j = 0$ . A metric on  $dE(M; \mathbb{R}^3)$  naturally induced by this construction is given by

$$\mathcal{G}_E(du_1, du_2) := \int_M \rho \langle u_1^0, u_2^0 \rangle_{\mathbb{R}^3} \mu, \quad du_1, du_2 \in d\Omega^0(M; \mathbb{R}^3), \quad (9)$$

where we identify tangent vectors with their principal parts.

As the configuration space  $\mathcal{V}(M; \mathbb{R}^3)$  is an open subset of  $\Omega^1(M; \mathbb{R}^3)$ , the tangent manifold  $T\mathcal{V}(M; \mathbb{R}^3)$  of  $\mathcal{V}(M; \mathbb{R}^3)$  is trivial

$$T\mathcal{V}(M; \mathbb{R}^3) = \mathcal{V}(M; \mathbb{R}^3) \times \Omega^1(M; \mathbb{R}^3).$$

Applying Theorem 2.1, tangent vectors  $\eta \in T\mathcal{V}(M; \mathbb{R}^3)$  allows to equip the configuration space  $\mathcal{V}(M; \mathbb{R}^3)$  with a metric as follows.

**Definition 4.1** Let  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$  be an arbitrary generalised configuration. For each pair  $\eta_i \in T_\gamma \mathcal{V}(M; \mathbb{R}^3)$ ,  $i = 1, 2$ , let

$$\eta_i = du_i + v_i \quad \text{with} \quad du_i \in d\Omega^0(M; \mathbb{R}^3), \quad v_i \in \mathcal{D}(M; \mathbb{R}^3)$$

be the respective Helmholtz decompositions. A metric  $\mathcal{G}_\gamma$  on the configuration space  $\mathcal{V}(M; \mathbb{R}^3)$  is defined by setting

$$\mathcal{G}_\gamma[\gamma](\eta_1, \eta_2) := \mathcal{G}_\gamma^{(e)}[\gamma](du_1, du_2) + \mathcal{G}_\gamma^{(p)}[\gamma](v_1, v_2).$$

The *elastic* part of  $\mathcal{G}^{(e)}$  is given by

$$\mathcal{G}_\gamma^{(e)}[\gamma](du_1, du_2) := \mathcal{G}_E(du_1, du_2), \quad du_1, du_2 \in d\Omega^0(M; \mathbb{R}^3),$$

where  $\mathcal{G}_E$  is defined in (9). The *plastic* part of  $\mathcal{G}_\gamma$  is given by

$$\mathcal{G}_\gamma^{(p)}[\gamma](v_1, v_2) := \int_M \sigma \langle v_1, v_2 \rangle \mu, \quad v_1, v_2 \in \mathcal{D}(M; \mathbb{R}^3),$$

where  $\sigma \in C^\infty(M)$  is a strictly positive real-valued function.

Notice that physically, the function  $\sigma$  appearing in the above metric may be thought of as the density of inertia of the dislocations. For sake of simplicity we assume that the density  $\sigma$  is independent of the actual configuration. This means that all dislocations respond to a force action by the same specific inertia.

Let  $T\tau_\gamma : T^2\mathcal{V}(M; \mathbb{R}^3) \longrightarrow T\mathcal{V}(M; \mathbb{R}^3)$  denote the tangent map of the canonical projection  $\tau_\gamma$  and  $V(T\mathcal{V}(M; \mathbb{R}^3)) := \ker T\tau_\gamma$  the vertical bundle. Moreover, let  $V\mathcal{X} \in V(T\mathcal{V}(M; \mathbb{R}^3))$  denote the vertical component of any vector  $\mathcal{X} \in T^2\mathcal{V}(M; \mathbb{R}^3)$ . The metric  $\mathcal{G}_\gamma$  given in Definition 4.1 defines a natural weakly nondegenerate symplectic two-form  $\Omega$  on  $T\mathcal{V}(M; \mathbb{R}^3)$  by

$$\Omega[\xi](\mathcal{X}, \mathcal{Y}) := \mathcal{G}_\gamma[\gamma](V\mathcal{Y}, T\tau_\gamma \mathcal{X}) - \mathcal{G}_\gamma[\gamma](V\mathcal{X}, T\tau_\gamma \mathcal{Y}) \quad (10)$$

for all  $\mathcal{X}, \mathcal{Y} \in T_\xi T\mathcal{V}(M; \mathbb{R}^3)$ ,  $\xi \in T_\gamma \mathcal{V}(M; \mathbb{R}^3)$ ,  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$ . Thus,  $T\mathcal{V}(M; \mathbb{R}^3)$  endowed with  $\Omega$  becomes a symplectic manifold. Since  $T\mathcal{V}(M; \mathbb{R}^3)$  is trivial, in coordinates one has

$$\mathcal{X} = (\gamma, \xi, \xi_1, \xi_2) \quad \text{and} \quad \mathcal{Y} = (\gamma, \xi, \eta_1, \eta_2)$$

which in turn yields

$$\Omega[\gamma, \xi](\xi_1, \xi_2, \eta_1, \eta_2) = \mathcal{G}_\gamma[\gamma](\eta_2, \xi_1) - \mathcal{G}_\gamma[\gamma](\xi_2, \eta_1).$$

The metric  $\mathcal{G}_\nu$  induces the kinetic energy functional  $\mathcal{E} : TV(M; \mathbb{R}^3) \rightarrow \mathbb{R}$  of the dislocated material by setting

$$\mathcal{E}(\xi) := \frac{1}{2} \mathcal{G}_\nu[\gamma](\xi, \xi), \quad \xi \in T_\gamma \mathcal{V}(M; \mathbb{R}^3), \quad \gamma \in \mathcal{V}(M; \mathbb{R}^3). \quad (11)$$

If  $\xi = du + v$  denotes the Helmholtz decomposition, then, according to Definition 4.1, the kinetic energy  $\mathcal{E}$  of a dislocated material splits into an *elastic part*

$$\mathcal{E}^{(e)}(\xi) := \frac{1}{2} \mathcal{G}_\nu^{(e)}[\gamma](du, du),$$

corresponding to the kinetic energy associated with the material mass density, and into a *plastic part*

$$\mathcal{E}^{(p)}(\xi) := \frac{1}{2} \mathcal{G}_\nu^{(p)}[\gamma](v, v),$$

corresponding to the kinetic energy of the dislocation density. By construction, the metric  $\mathcal{G}_\nu$  is constant in  $\gamma$ , that is

$$D\mathcal{G}_\nu[\gamma](\eta) = 0 \quad \forall \eta \in T_\gamma \mathcal{V}(M; \mathbb{R}^3), \quad \gamma \in \mathcal{V}(M; \mathbb{R}^3).$$

Therefore, the corresponding Euler's equations yield

$$\mathcal{G}_\nu[\gamma(t)](\dot{\gamma}(t), \eta) = 0, \quad \forall \eta \in TV(M; \mathbb{R}^3)$$

as weak equations of motion. The geodesics of  $\mathcal{G}_\nu$  are analogously to elasticity straight line segments, cf. [4, 6]. An inertial motion follows by definition the geodesics of  $\mathcal{G}_\nu$ . A motion under non-vanishing forces will deviate from these geodesics.

## 5 The Principle of Virtual Work

In our setting, a work functional on the space of generalised configurations  $\mathcal{V}(M; \mathbb{R}^3)$  is understood to be a continuous linear functional

$$F : TV(M; \mathbb{R}^3) \cong \mathcal{V}(M; \mathbb{R}^3) \times \Omega^1(M; \mathbb{R}^3) \rightarrow \mathbb{R},$$

on the tangent bundle  $TV(M; \mathbb{R}^3)$ . We assume that for each configuration  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$  the functional  $F$  admits an integral representation with respect to the metric  $\mathcal{G}$  given in (2), such that

$$F[\gamma](\eta) = \int_M \langle \alpha[\gamma], \eta \rangle \mu \quad \forall \eta \in T_\gamma \mathcal{V}(M; \mathbb{R}^3). \quad (12)$$

The *constitutive law* of the continuum  $M$  is encoded in the functional dependence of the integral kernel  $\alpha[\gamma] \in \Omega^1(M; \mathbb{R}^3)$  on the configuration  $\gamma$ . This dependence will, in

general, be non-linear and possibly also non-local. More precisely, the integral kernel  $\alpha$  may be thought of as a smooth section into the tangent bundle  $T\mathcal{V}(M; \mathbb{R}^3)$ , where each  $\alpha[\gamma]$  is identified with its principal part. The one-form  $\alpha$  will be called *stress form*; in classical elasticity,  $\alpha$  corresponds to the *first Piola-Kirchhoff* stress tensor, cf. [5, 16].

For each  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$ , the Helmholtz decomposition of  $\alpha[\gamma]$  reads

$$\alpha[\gamma] = dh[\gamma] + \tau[\gamma], \quad (13)$$

where  $dh[\gamma] \in d\Omega^0(M; \mathbb{R}^3)$  is a gradient and  $\tau[\gamma] \in \mathcal{D}(M; \mathbb{R}^3)$  is divergence-free. The decompositions are understood with respect to a fixed reference metric  $g$ . Writing  $\eta = du + v$ , the orthogonality of the Helmholtz decomposition implies

$$\mathcal{G}(\alpha[\gamma], \eta) = \mathcal{G}(dh[\gamma], du) + \mathcal{G}(\tau[\gamma], v).$$

Therefore, for each generalised configuration  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$ , the work functional  $F$  splits into an *elastic part*  $F^{(e)}$  and a *plastic part*  $F^{(p)}$ , i.e.

$$F[\gamma](\eta) = F^{(e)}[\gamma](du) + F^{(p)}[\gamma](v) \quad \forall \eta = du + v \in T_\gamma \mathcal{V}(M; \mathbb{R}^3). \quad (14)$$

The elastic part is given by

$$F^{(e)}[\gamma](du) := \int_M \langle dh[\gamma], du \rangle \mu \quad \forall du \in d\Omega^0(M; \mathbb{R}^3), \quad (15)$$

and the plastic part by

$$F^{(p)}[\gamma](v) := \int_M \langle \tau[\gamma], v \rangle \mu \quad \forall v \in \mathcal{D}(M; \mathbb{R}^3). \quad (16)$$

Since the Helmholtz decomposition is orthogonal,

$$F = F^{(e)} \iff \alpha[\gamma] = dh[\gamma] \quad \forall \gamma \in \mathcal{V}(M; \mathbb{R}^3).$$

It was first observed in [3] that in pure elasticity, only the exact part  $dh[\gamma]$  of the stress form  $\alpha[\gamma]$  contributes to the work functional. In fact,  $F^{(e)}$  is the well-known work functional of elasticity, cf. [1, 7, 14]. The work functional (12) thus becomes a natural generalisation of the notion of work in classical elasticity.

Notice that both components  $dh[\gamma]$  and  $\tau[\gamma]$  of the stress form  $\alpha[\gamma] = dh[\gamma] + \tau[\gamma]$  will, in general, depend on the integrable part  $dj$  as well as the plastic part  $\beta \in \mathcal{D}(M; \mathbb{R}^3)$  of  $\gamma = dj + \beta$ . From the elastic point of view,  $\tau$  marks a gauge freedom, cf. [5]. Hence, the choice of  $\tau$  describes the plastic part in view.

Next, we implement the work functional (12) in the d'Alembert principle of virtual work. According to [13], an exterior force acting on a general mechanical system is given by a horizontal one-form on the tangent manifold of the corresponding configuration space.

Recall that, using the tangent map  $T\tau_V : T^2\mathcal{V}(M; \mathbb{R}^3) \rightarrow T\mathcal{V}(M; \mathbb{R}^3)$  of the canonical projection  $\tau_V$ , a vector field  $\mathcal{Y}$  on  $T\mathcal{V}(M; \mathbb{R}^3)$  is by definition *vertical* iff  $T\tau_V(\mathcal{Y}) = 0$ . A one-form  $\mathcal{F}$  on  $T\mathcal{V}(M; \mathbb{R}^3)$  is *horizontal* iff  $\mathcal{F}(\mathcal{Y}) = 0$  for all vertical vector fields  $\mathcal{Y}$ . Thus, an exterior force in the above sense acting on dislocated material is given by a horizontal one-form  $\mathcal{F}$  on  $T\mathcal{V}(M; \mathbb{R}^3)$ .

If  $\mathcal{Y}$  is a vertical vector field and  $\Omega$  is the symplectic two-form defined in (10), then

$$\Omega(\mathcal{Y}, \mathcal{Z}) = -\mathcal{G}_V[\gamma](\mathcal{Y}, T\tau_V\mathcal{Z}) \quad \forall \mathcal{Z} \in \Gamma(T^2\mathcal{V}(M; \mathbb{R}^3)).$$

Therefore, the induced one-form  $\iota_{\mathcal{Y}}\Omega$  given by

$$\iota_{\mathcal{Y}}\Omega(\mathcal{Z}) := \Omega(\mathcal{Y}, \mathcal{Z}) \quad \forall \mathcal{Z} \in \Gamma(T^2\mathcal{V}(M; \mathbb{R}^3))$$

is horizontal<sup>2</sup>. On the other hand, using the tangent map  $T\tau_V$  of the canonical projection  $\tau_V$ , the work functional  $F$  defined in (12) induces an exterior work one-form  $\mathcal{F}$  in the above sense by setting

$$\mathcal{F} := (T\tau_V)^*F. \quad (17)$$

Due to the pull-back construction,  $\mathcal{F}$  is horizontal. Given the kinetic energy functional  $\mathcal{E}$  and an exterior work one-form (17), the d'Alembert principle of virtual work now states that the Euler vector field  $\mathcal{X}$  is determined by the equation

$$d\mathcal{E}(\mathcal{Z}) - \iota_{\mathcal{X}}\Omega(\mathcal{Z}) = (T\tau_V)^*F(\mathcal{Z}) \quad \forall \mathcal{Z} \in \Gamma(T^2\mathcal{V}(M; \mathbb{R}^3)). \quad (18)$$

## 6 The Equations of Motion

In order to formulate a dynamics on our configuration space  $\mathcal{V}(M; \mathbb{R}^3)$ , consider a motion given by a smooth curve

$$\gamma : \mathbb{R} \rightarrow \mathcal{V}(M; \mathbb{R}^3), \quad t \mapsto \gamma(t).$$

Using the exterior work functional (17), the curve  $\gamma(t)$  describes a motion subject to the d'Alembert principle of virtual work (18), if it satisfies the weak equations of motion

$$\mathcal{G}_V[\gamma(t)](\ddot{\gamma}(t), \eta) = F[\gamma(t)](\eta) \quad \forall \eta \in \Omega^1(M; \mathbb{R}^3). \quad (19)$$

According to Helmholtz, each  $\gamma(t)$ ,  $t \in \mathbb{R}$  decomposes into  $\gamma(t) = dj(t) + \beta(t)$ . The orthogonality of the splittings of the work functional  $F = F^{(e)} + F^{(p)}$  and the metric

<sup>2</sup>In the case where  $\Omega$  is regular, the converse also holds true: for any horizontal one-form  $\mathcal{F}$ , there is a vertical vector field  $\mathcal{Y}_{\mathcal{F}}$  such that  $\mathcal{F} = \iota_{\mathcal{Y}_{\mathcal{F}}}\Omega$ .

$\mathcal{G}_V = \mathcal{G}_V^{(e)} + \mathcal{G}_V^{(p)}$  given in Definition 4.1, respectively, implies that (19) is equivalent to the system of equations

$$\mathcal{G}_V^{(e)}[\gamma(t)](dj(t), du) = F^{(e)}[\gamma(t)](du) \quad \forall du \in d\Omega^0(M; \mathbb{R}^3) \quad (20)$$

and

$$\mathcal{G}_V^{(p)}[\gamma(t)](\dot{\beta}(t), v) = F^{(p)}[\gamma(t)](v) \quad \forall v \in \mathcal{D}(M; \mathbb{R}^3). \quad (21)$$

Thus, the dynamical equations derived from the principle of virtual work split into an *elastic part* (20) and into a *plastic part* (21). In absence of all external volume and surface forces, the equations of motion<sup>3</sup> induced by (20) and (21) are given in the following theorem.

**Theorem 6.1** Let  $\alpha[\gamma] = dh[\gamma] + \tau[\gamma]$  be the Helmholtz decomposition of a stress form for a dislocated material. Then the equations of motion are given by

$$\begin{cases} \rho \ddot{j}(t) &= \Delta h[\gamma(t)] \\ \sigma \ddot{\beta}(t) &= \tau[\gamma(t)] \end{cases},$$

where  $\gamma(t) = dj(t) + \beta(t)$  is the Helmholtz decomposition of  $\gamma(t)$  and  $\Delta := \delta \circ d$  is the Laplace operator on functions in  $C^\infty(M; \mathbb{R}^3)$ .

The first equation in Theorem 6.1 is nothing but the well-known equation of motion in elasticity: since  $\delta\tau[\gamma] = 0$ , the divergence of the stress form  $\alpha[\gamma]$  corresponding to the first Piola-Kirchhoff stress tensor can be represented as the Laplace operator on functions, i.e.  $\delta\alpha[\gamma] = \Delta h[\gamma]$ . The second one is an evolution equation for the non-integrable parts of the deformation  $\gamma(t)$ . The equations of motion are coupled via the Helmholtz decomposition. The motion of dislocations may, in general, be accompanied by dissipative effects, cf. [11].

In a static setting,  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$  is an equilibrium configuration if and only if

$$F[\gamma](\eta) = 0 \quad \forall \eta \in T_\gamma \mathcal{V}(M; \mathbb{R}^3)$$

which according to (14) is equivalent to

$$F^{(e)}[\gamma](du) = 0 \quad \forall du \in d\Omega^0(M; \mathbb{R}^3) \quad \text{and} \quad F^{(p)}[\gamma](v) = 0 \quad \forall v \in \mathcal{D}(M; \mathbb{R}^3).$$

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<sup>3</sup>The equivalence of the weak equations and the strong equations follow from the fact, that the space of smooth differential forms is dense in an appropriate  $L^2$ -completion, cf. [17].

The *second Piola-Kirchhoff* stress tensor  $\mathbf{S}[\gamma]$  associated with the stress form  $\alpha[\gamma] \in \Omega^1(M; \mathbb{R}^3)$ ,  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$  is given by

$$\mathbf{S}[\gamma](X, Y) := \langle \alpha[\gamma](X), \gamma(Y) \rangle_{\mathbb{R}^3}, \quad X, Y \in \Gamma(TM).$$

In pure elasticity, there is a gauge freedom in choosing the stress form. Since only the integrable part  $dh[\gamma]$  of a stress form  $\alpha[\gamma]$  contributes to the work functional of elasticity  $F^{(e)}$ , any stress form  $\tilde{\alpha}[\gamma] = \alpha[\gamma] + \xi[\gamma]$  with arbitrary  $\xi[\gamma] \in \mathcal{D}(M; \mathbb{R}^3)$  will give the same work functional  $F^{(e)}$  and hence determine the same dynamics of the system, cf. [3]. In particular, one may choose  $\xi[\gamma]$  such that the stress tensor  $\tilde{\mathbf{S}}$  corresponding to  $\tilde{\alpha}[\gamma]$  is symmetric, cf. [16].

In the dislocated case, this gauge freedom is lost. Since the divergence-free part  $\tau$  of the stress form  $\alpha$  appears explicitly in the principle of virtual work (19), the stress tensor may not be chosen to be symmetric. The concept of decomposing configurations  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$  and stress forms  $\alpha[\gamma] \in \Omega^1(M; \mathbb{R}^3)$ ,  $\gamma \in \mathcal{V}(M; \mathbb{R}^3)$  is completely analogous to the concept of strain spaces and stress spaces in [10]. The integrable part of the deformation is the dual quantity to the integrable part of the stress, the non-integrable part of the deformation is the dual quantity to the non-integrable part of the stress.

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